

## Optimized tri-band MIMO antenna design for 6G terahertz applications and future connectivity

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### ABSTRACT

This paper presents an industrial and innovation rectangular-shaped multiple input multiple output (MIMO) antenna designed for terahertz (THz) frequency applications, specifically targeting 6G communication. The proposed antenna achieves triple-band operation at 3.62 THz, 6.248 THz, and 7.613 THz by incorporating four T-shaped slots. It is designed on a polyimide substrate with a dielectric constant of 3.5 and a tangent loss of 0.0027, with dimensions of 80  $\mu\text{m}$  by 180  $\mu\text{m}$  and a thickness of 11  $\mu\text{m}$ . The patch and the ground plane are constructed from copper, ensuring robust performance. The antenna provides bandwidths of 0.7 THz, 2.2 THz, and 1.1 THz, with isolation levels exceeding -31.3 dB. It achieves a peak gain of 14.3 dB and a high efficiency of 94%, demonstrating its potential for high-performance THz applications. MIMO performance parameters, such as the envelope correlation coefficient (ECC), diversity gain (DG), mean effective gain (MEG), and total active reflection coefficient (TARC), exhibit excellent agreement with theoretical values. The design is further validated through simulations using computer simulation technology (CST) and a circuit model in advanced design system (ADS). The results of these tests mirrored those of the CST simulations, confirming the reliability of future 6G THz communication systems.

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## 1. INTRODUCTION

The evolution of wireless communication technology is rapidly progressing towards 6G, aiming to fulfil the increasing demand for high data rates, ultra-low latency, and massive connectivity. A key enabler for 6G technology is the utilization of terahertz (THz) frequency bands, which offer unprecedented bandwidth capabilities for short-range wireless communication [1]. THz communication stands out because it can provide extremely high data transfer rates, making it ideal for applications such as high-definition video streaming, augmented reality, and advanced IoT networks [2]. THz frequencies, typically ranging from 0.1 to 10 THz, offer significantly higher bandwidth than traditional microwave and millimeter-wave frequencies [3]. This higher bandwidth translates to greater data transfer rates, which is essential for meeting future wireless applications' performance requirements. Short-range wireless communication, which involves distances typically within a few meters, benefits immensely from THz technology because it can handle large

volumes of data with minimal latency [4]. However, using THz frequencies introduces challenges, such as high path loss, limited penetration capabilities, and susceptibility to atmospheric absorption. It is imperative that these issues be addressed for practically deploying THz communication systems [5].

Incorporating multiple input multiple output (MIMO) technology with THz communication further enhances performance by leveraging spatial diversity to improve signal strength and data throughput [6]. Simultaneous transmission and reception of various data streams is made possible by MIMO technology, which use a number of antennas on both the transmitter and the receiver. This spatial multiplexing capability significantly increases wireless communication systems' capacity and spectral efficiency [7]. The combination of THz communication with MIMO systems is poised to overcome the limitations of traditional communication systems by significantly increasing capacity and spectral efficiency [8]. This synergy is crucial for realizing the full potential of 6G technology, as it supports a wide range of applications requiring ultra-fast and reliable wireless connections [9]. The integration of THz communication and MIMO technology represents a significant advancement in wireless communication. As the demand for higher data rates and more reliable connections continues to grow, system development will play a critical role in shaping the future of 6G technology, ensuring seamless connectivity and enhanced user experiences in short-range wireless communication environments [10].

A comparative study of several MIMO antenna designs is shown in Table 1, focusing on their fundamental parameters and performance metrics. The proposed antenna design stands out with its remarkable performance across these parameters, showcasing significant advancements in antenna technology and setting a new standard for comparison.

Bandwidth values show considerable variation, with measurements including 0.05 THz, 0.114 THz, 0.038 THz, 0.3 THz, 0.78 THz, and 0.4 THz at [11], [12]. In contrast, the proposed design achieves significantly broader bandwidths of 0.7 THz, 2.2 THz, and 1.1 THz at its three resonance frequencies of 3.62 THz, 6.248 THz, and 7.61 THz, respectively. The gain values reported in the references are 11.67 dB, 4.4 dB, 5 dB, 10 dB, 4.4 dB, and 5.49 dB [11], [12]. The proposed design, however, achieves substantially higher gains of 13.5 dB, 14.3 dB, and 13.9 dB at its three resonance frequencies. Isolation is another critical factor in which the proposed design excels. The referenced antennas exhibit isolation values of -25 dB, -17 dB, -17 dB, -35 dB, -20 dB, and -25 dB at [11], [12]. In comparison, the proposed antenna achieves isolation levels of -33.32 dB, -30.01 dB, and -35.27 dB across its three bands. In terms of efficiency, the proposed antenna also outperforms the referenced designs. The efficiencies reported in the references are 76.45%, 94%, 60%, 96%, and 85.24% [11]-[14]. The proposed antenna achieves efficiencies of 93.77%, 95.2%, and 93.79% at its three operating frequencies. The suggested MIMO antenna performed exceptionally well compared to other options, with an ECC <0.0007 and a diversity gain (DG) above 9.996. Notably, whereas references [14], [15], used resistor, inductor, and capacitor (RLC) circuits, the suggested antenna incorporates RLC components to evaluate its electromagnetic behaviour, distinguishing it and emphasizing its novel approach. These attributes together demonstrate the suggested antenna's ability to lead the field of antenna technology and drive future developments, making it the best of the compared designs.

Table 1. Performance metrics comparison of proposed MIMO antenna and existing designs

Ref	Resonance (THz)	BW (THz)	Isolation (dB)	Gain (dB)	Efficiency (%)	ECC, DG (dB)	Substrate material	Port	RLC
[11]	0.654	0.05	-25	11.67	76.45%	0.003, 9.99	polyimide	-	No
[16]	-	0.114	-17	4.4	94	0.006, 9.97	Rogers RO4835-T	4	No
[13]	2.3, 3.2, 4.5	0.038, 0.043, 0.06	-17, -30, -23	5	60%	0.2, 10	Polyimide	2	No
[15]	1.9	0.3	-35	10	-	0.00002 3/9.99	Polyimide	2	Yes
[14]	2.2	0.78	-20	4.4	96	0.006, 9.9998	Polyimide	2	Yes
[12]	-	0.4	-25	5.49	85.24	0.015/ 9.99	Polyimide	2	No
Proposed	3.62, 6.24, 7.61	0.7, 2.2, 1.1	-33.32, -30.01, -35.27	13.5, 14.3, 13.9	93.77, 95.2, 93.79	0.0007, 9.996	Polyimide	2	Yes

## 2. ITERATIVE DESIGN AND ANALYSIS OF THE SINGLE-ELEMENT ANTENNA

In our endeavour to engineer a cutting-edge antenna for THz applications, we meticulously designed a single-element antenna, refining its architecture through three progressive stages to attain optimal

performance. The final design of this antenna is presented in Figure 1, which shows Figure 1(a) presenting a 3D view, Figure 1(b) showcasing the side view, Figure 1(c) displaying the front view, and Figure 1(d) highlighting the back view.

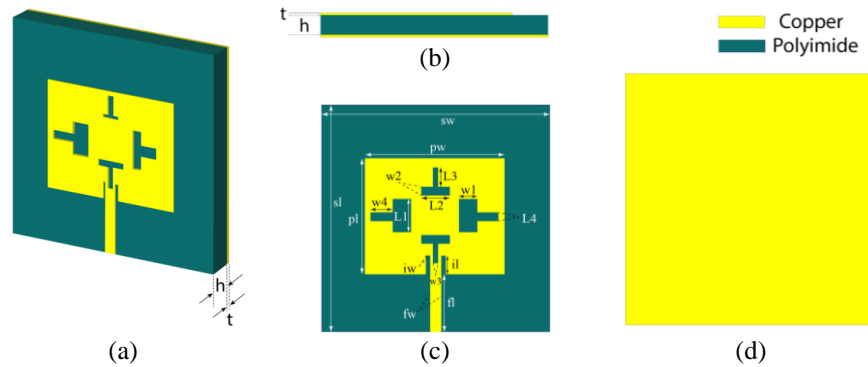


Figure 1. Antenna configuration; (a) 3D perspective view, (b) side view, (c) front view, and (d) back view

Polyimide is chosen as the substrate due to its superior dielectric properties, boasting a dielectric constant of 3.5 and a low-loss tangent of 0.0027 [17]. This strategic choice reassures us of the robustness and reliability of our design. Copper was employed for both the patch and ground elements to maximize conductivity, thereby enhancing signal grounding and radiation efficiency. The design consistently featured a full ground plane, ensuring robust performance. In (1) and (2) were used to calculate the antenna's measurements [18].

$$W = \frac{c}{2f} \times \sqrt{\frac{2}{\epsilon_r + 1}} \quad (1)$$

$$L = \frac{c}{(2f\sqrt{\epsilon_{eff}})} - 2 \times \Delta L \quad (2)$$

The antenna's reflection coefficient across each design stage is demonstrated in Figure 2(a), while Figure 2(b) depicts the corresponding gain. In the initial design, a facile rectangular patch antenna with a feedline and two symmetrical rectangular slots was used. This configuration produced two resonance frequencies, but the performance was subpar, particularly in return loss, and gain. To address these issues, further design refinements were pursued in the next stage. Building upon the foundational design, in the second stage two rectangular slots were added above and below the central section of the patch, and insets were introduced on both sides of the feedline. This refinement resulted in dual-band frequencies at 3.81 THz and 6.5 THz, with improved return losses of -21.44 dB and -34.36 dB, respectively. The gain also showed notable improvement, although there remained potential for further optimization. In the final design, we incorporated small extensions, akin to arms, on the sides of the rectangular slots. This enhancement resulted in three distinct resonance frequencies at 3.75 THz, 6.38 THz, and 7.74 THz, with impressive return losses of -26.54 dB, -50.5 dB, and -38.5 dB, respectively. The antenna's peak gain was recorded at 11.7 dB, underscoring its reliability and efficiency. Additionally, the antenna achieved substantial bandwidths of 0.5 THz, 1 THz, and 0.63 THz at its three operating frequencies. These exceptional performance characteristics underscore the antenna's viability for integration into advanced 6G communication systems.

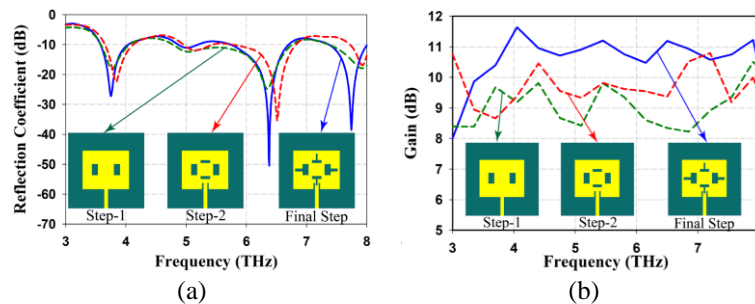


Figure 2. Performance analysis of the single-element antenna design; (a) S11 comparison and (b) Gain comparison

### 3. DESIGN AND ANALYSIS OF THE MIMO ANTENNA

MIMO antennas offer substantial advantages over single-element designs, including enhanced system capacity, improved data throughput, and superior signal quality. MIMO antennae can deliver higher performance by exploiting spatial diversity and reducing interference. Especially in complex communication environments [19].

In this section, we describe the progression of a 2-port MIMO antenna, evolving from a single-element design to enhance overall performance. Figure 3(a) illustrates the MIMO antenna configuration, featuring two elements placed side by side with a 180-degree orientation relative to each other. The antennas are spaced  $40\text{ }\mu\text{m}$  apart edge-to-edge, within an overall dimension of  $80\times 180\text{ }\mu\text{m}$ . This arrangement is designed to maximize spatial diversity and minimize mutual coupling, thereby optimizing signal quality and reliability. Following implementing the MIMO configuration, we identified three distinct resonance frequencies at 3.62 THz, 6.24 THz, and 7.61 THz. The bandwidths achieved are 0.7 THz, 2.2 THz, and 1.1 THz at its three operating frequencies, as displayed in Figure 3(b). Additionally, Figure 3(c) highlights a maximum gain of 14.3 dB. Figures 3(b) and (c) provide a comparative analysis of return loss and gain respectively between the single-element and MIMO antenna. These figures demonstrate that the MIMO antenna offers markedly superior performance compared to the single-element antenna.

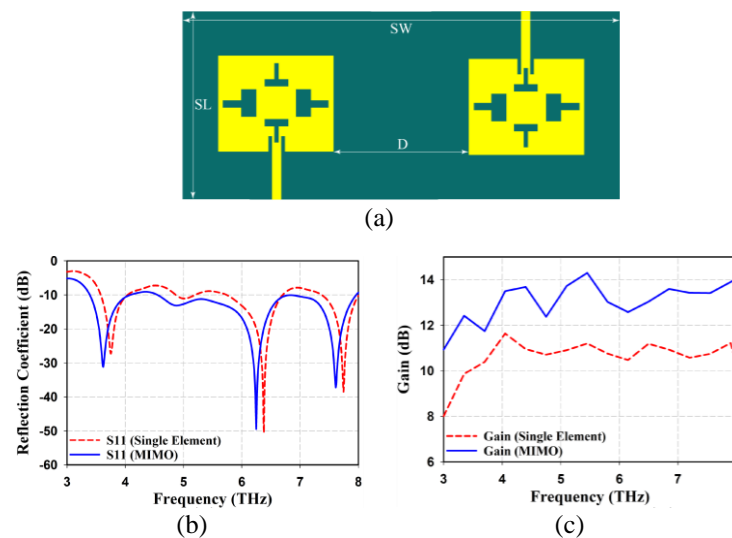


Figure 3. Performance comparison of single-element and MIMO antenna; (a) MIMO antenna design, (b) S11 parameter comparison, and (c) gain comparison

These values represent the ideal setting of the antenna,  $sw=70\text{ }\mu\text{m}$ ,  $sl=80\text{ }\mu\text{m}$ ,  $pw=45\text{ }\mu\text{m}$ ,  $pl=40\text{ }\mu\text{m}$ ,  $L1=12\text{ }\mu\text{m}$ ,  $L2=10\text{ }\mu\text{m}$ ,  $L3=7\text{ }\mu\text{m}$ ,  $L4=3\text{ }\mu\text{m}$ ,  $w1=6\text{ }\mu\text{m}$ ,  $w2=3\text{ }\mu\text{m}$ ,  $w3=2\text{ }\mu\text{m}$ ,  $w4=8\text{ }\mu\text{m}$ ,  $iw=1\text{ }\mu\text{m}$ ,  $il=6\text{ }\mu\text{m}$ ,  $fl=20\text{ }\mu\text{m}$ ,  $fw=4\text{ }\mu\text{m}$ ,  $h=11\text{ }\mu\text{m}$ ,  $t=0.5\text{ }\mu\text{m}$ ,  $D=40\text{ }\mu\text{m}$ ,  $SW=180\text{ }\mu\text{m}$ , and  $SL=80\text{ }\mu\text{m}$ .

### 4. RESULTS ANALYSIS OF THE RECOMMENDED MIMO ANTENNA

#### 4.1. Reflection coefficient and transmission coefficient analysis

The reflection coefficient measures how much power is reflected back from the antenna, with lower values indicating better impedance matching [20]. Figure 4(a) illustrates that the proposed MIMO antenna achieves triple-band operation, resonating at three distinct frequencies: 3.62 THz, 6.248 THz, and 7.61 THz. The return losses at these resonance frequencies are -31.114 dB, -49.45 dB, and -37.22 dB, respectively, indicating excellent impedance matching. The first band operates between 3.39 THz and 4.09 THz, providing a bandwidth of 0.7 THz. The second band spans from 4.56 THz to 6.76 THz, resulting in a high bandwidth of 2.2 THz. The third band operates between 6.76 THz and 7.86 THz, with a bandwidth of 1.1 THz. These wide bandwidths ensure the antenna's capability to support a broad range of frequencies, making it highly suitable for advanced THz applications.

Isolation or transmission coefficient is crucial in MIMO systems, showing how much the antenna parts interact with one another [21]. The proposed antenna achieves a very high isolation value of -30.01 dB (shown in Figure 4(b)). Which is excellent and suggests that the antenna elements are well-isolated, reducing cross-talk and enhancing overall system performance [22].

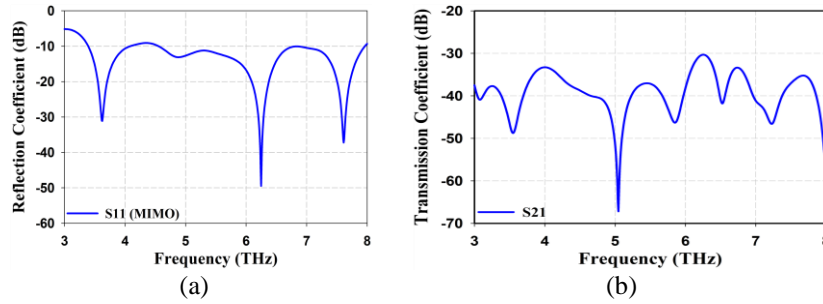


Figure 4. Performance analysis of the proposed MIMO antenna; (a) reflection and (b) transmission coefficient

#### 4.2. Gain and efficiency

Gain and efficiency are essential metrics for evaluating antenna performance. Gain refers to the ability of an antenna to direct radiated energy in a particular direction, which enhances signal strength and improves communication range [23], [24]. Efficiency represents the effectiveness of an antenna in converting input power into radiated energy with minimal losses [25]. Figure 5 depicts a plot of the simulated gain and Efficiency of the suggested antenna. The proposed antenna achieves maximum gains of 13.5 dB, 14.3 dB, and 13.9 dB at the respective bands of 3.62 THz, 6.248 THz, and 7.61 THz. These high gain values indicate the antenna's ability to direct energy efficiently, which is crucial for long-distance communication. Additionally, the antenna maintains high efficiencies of 92%, 94%, and 93% at the three respective bands. This high efficiency indicates that the antenna effectively converts input power into radiated energy with minimal losses, optimizing overall performance [26].

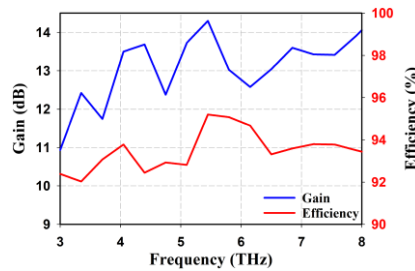


Figure 5. Gain and efficiency of the proposed THz MIMO antenna

#### 4.3. Diversity performance analysis

The diversity performance of the proposed antenna is assessed using the envelope correlation coefficient (ECC), DG, mean effective gain (MEG), total active reflection coefficient (TARC) [27]. The ECC indicates how similar or different the signals received by the different antennas are. The value of ECC can be figured out by using the expression shown in (3) [28]:

$$\frac{|\int_{4\pi} [E_1(\theta, \varphi) \cdot E_2^*(\theta, \varphi)] d\Omega|^2}{\int_{4\pi} |E_1(\theta, \varphi)|^2 d\Omega \int_{4\pi} |E_2(\theta, \varphi)|^2 d\Omega} \quad (3)$$

The antenna achieves an ECC value of 0.00004, which is exceptionally low and desirable, as shown in Figure 6(a). This low ECC enhances the antenna's ability to provide multiple independent signal paths, improving signal quality and reliability.

The DG, which measures the improvement in signal quality achieved through diversity, is nearly ideal at 9.99999, as shown in the same figure of ECC (Figure 6(a)). The value of DG can be determined by using the equation provided here [29].

$$DG = 10\sqrt{1 - ECC^2} \quad (4)$$

This high DG value, confirms the excellent diversity performance of the antenna, ensuring robust communication even in challenging environments.

In Figure 6(b), the TARC plot shows weighty dips at the operational frequencies (3.62 THz, 6.248 THz, and 7.613 THz), signifying good impedance matching and low reflection, critical for efficient antenna performance in 6G THz applications. In (3) can be utilised to ascertain this [30].

$$TARC = \frac{\sqrt{(|S_{xx}|+|S_{xy}|)^2+(|S_{yx}|+|S_{yy}|)^2}}{\sqrt{4}} \quad (5)$$

In Figure 6(c), the MEG plot for the two MIMO antenna ports (MEG 1 and MEG 2) are meticulously associated and relatively constant across the frequency range, prominence well-adjusted performance and good signal response, important for accomplishing high DG and low correlation in MIMO systems. It can be mathematically represented as (6) and (7) [31]:

$$k = \min\left(\frac{MEG_1}{MEG_2}, \frac{MEG_2}{MEG_1}\right) \quad (6)$$

$$MEG_i = 0.5 \left[ 1 - \sum_{j=1}^N S_{ij} \right] \quad (7)$$

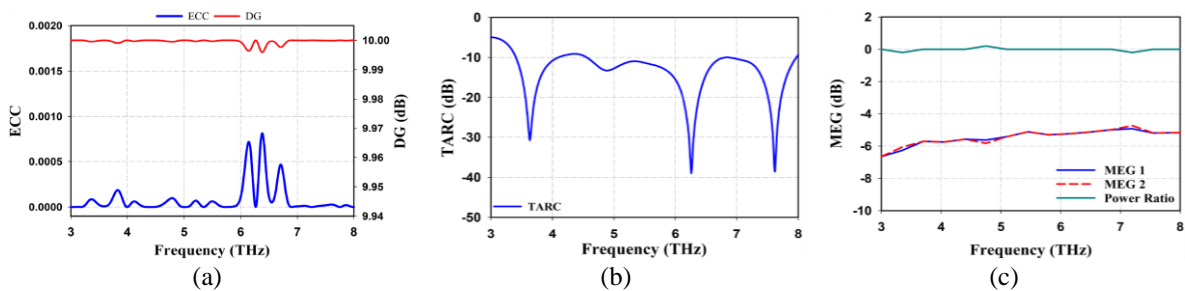


Figure 6. Diversity performance; (a) ECC and DG, (b) TARC, and (c) MEG of the MIMO antenna

#### 4.4. Radiation pattern

The radiation pattern analysis of the proposed antenna at 6.5 THz, illustrated in Figure 7, reveals notable E-field and H-field characteristics. At  $\phi=0^\circ$ , the E-field displays a main lobe magnitude of 11.1 dBV/m with a 3 dB beamwidth of 41.7 degrees, whereas the H-field shows a main lobe magnitude of -37.9 dBA/m and a beamwidth of 17.3 degrees. In the  $\phi=90^\circ$  plane, the E-field's main lobe magnitude is 8.73 dBV/m with a 3 dB beamwidth of 15.6 degrees, while the H-field presents a magnitude of -26.8 dBA/m and a beamwidth of 33.5 degrees. Additionally, for  $\theta=90^\circ$ , the E-field achieves a main lobe magnitude of 24.8 dBV/m with a beamwidth of 28.5 degrees, and the H-field has a magnitude of -39.1 dBA/m with a 3 dB beamwidth of 8.7 degrees. These patterns, demonstrate the antenna's capability to deliver efficient directional radiation across different planes at its operating frequency [32].

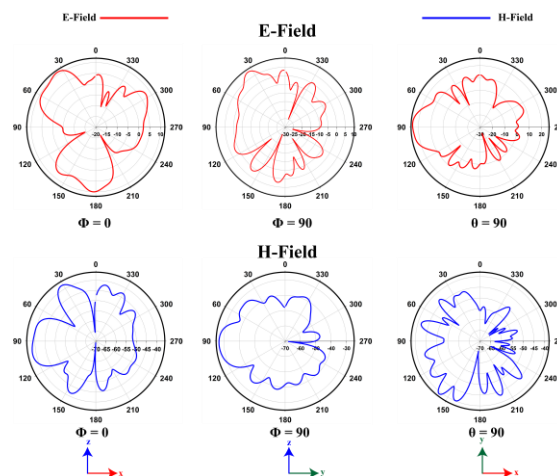


Figure 7. Simulated radiation pattern

## 5. EQUIVALENT CIRCUIT MODELING

To advance our antenna technology, we meticulously analyzed the electromagnetic behavior of our antenna using an R-L-C circuit model. The R-L-C parameters were precisely extracted from CST Studio simulations, which we further refined through circuit simulations in Agilent advanced design system (ADS), enabling a comprehensive performance assessment [33]. During the RLC equivalent circuit design, we employed a trial-and-error approach using ADS software, iteratively adjusting the RLC parameters to achieve optimal results.

In our antenna design process, we identified that the three resonance frequencies were primarily influenced by the four T-shaped slots. Consequently, we designed a plus-shaped circuit corresponding to these slots. Each T-shaped slot was modeled as a parallel circuit of resistance (R), capacitance (C), and inductance (L), connected in series with another resistance (R). These circuits were crucial in determining the antenna's resonance frequencies. Additionally, the capacitance between two adjacent T-shaped slots was represented by a series circuit of two capacitors. The feedline was also modeled with specific resistance ( $R_x$ ), capacitance ( $C_x$ ), and inductance ( $L_x$ ) parameters to accurately reflect its electrical properties. By integrating these circuit elements, we constructed a model that faithfully represented the behavior of our single-element antenna. We then extended this model to a MIMO antenna configuration, as shown in Figure 8, using the single-element circuit as a foundation. To adapt to the MIMO setup, we incorporated the mutual impedance between antenna elements using a parallel circuit composed of  $L_5$  and  $C_9$ . This approach optimized the performance evaluation. We validated the R-L-C circuit model through simulations in Agilent ADS, ensuring its alignment with our antenna design. To confirm its precision, we compared the CST simulation results with those obtained from the circuit simulation, focusing specifically on the  $S_{11}$  parameter. Figure 9 illustrates this comparison, providing a thorough evaluation of our R-L-C circuit model's accuracy in representing the antenna's behavior.

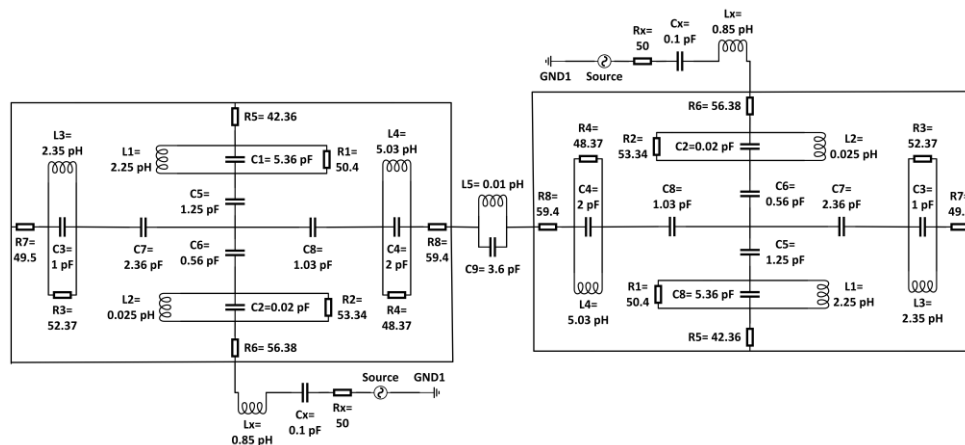


Figure 8. RLC equivalent circuit diagram for the suggested MIMO antenna

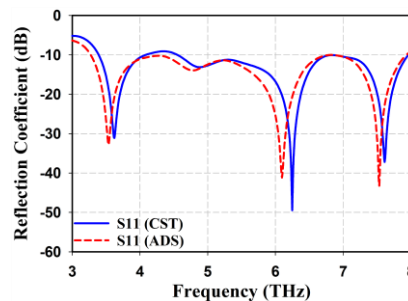


Figure 9. Comparative plot of  $S_{11}$  parameter from CST and ADS simulations

## 6. CONCLUSION

This research has thoroughly investigated a novel MIMO antenna adapted for THz applications, utilizing a range of analytical methods, including the creation of an RLC-equivalent circuit model. The performance of the proposed antenna was meticulously evaluated through both ADS and CST simulations,



demonstrating a remarkable consistency in bandwidth across these platforms. The antenna's design showcases exceptional performance characteristics, including broad bandwidth, high isolation, significant gain, and impressive efficiency. The isolation parameter effectively reduces mutual coupling among antenna elements, which is crucial for maintaining optimal performance in a MIMO system. Additionally, the antenna excels in diversity performance, evidenced by a very low ECC and an almost perfect DG, indicating its potential to deliver high-quality and reliable communication. The consistency of results obtained from different simulation environments underscores the robustness and reliability of the proposed design. Overall, the research validates the effectiveness of the MIMO antenna for advanced THz communication systems and provides a solid foundation for further developments and practical applications in next-generation communication technologies. This study not only highlights the antenna's impressive performance metrics but also provides precious insights into the design and evaluation of high-frequency communication systems.

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